THE COLLEGE OF NEW JERSEY CIVIL ENGINEERING

ABSTRACT:

The AISC Student Steel Bridge Supplemental Competition is a national competition that challenges students to design and analyze a scale model steel bridge and the corresponding construction of this bridge. The team designed a Pratt Truss consisting of 20-foot-long stringers, angled lateral bracing, and a total height of 4.87 feet. A "twist and lock" connection was created for the stringers and a sleeve connection for the overhead truss members. The "twist and lock" features a male and female connector where the male swings a "T-Slot" into the female connector. The sleeve connections feature a 1.75" diameter steel pipe with a 0.058" wall thickness, connecting to a sleeve with a 1.634" diameter and a 0.125" wall thickness. Using this design, calculations were completed to estimate vertical deflection, buckling, and other items to ensure stability of the bridge. Overall, this design has a maximum vertical deflection of 0.56", a weight of 240 lbs., 57 members, and 50 connections. In total the final engineering cost for this project has been approximately \$122,000.00 with an estimated construction cost of \$3,500.

As of April 16, 2020, AISC announced that TCNJ's submission finished first overall in the Metropolitan region ahead of Rutgers University and New York University, and will move on to compete in the national competition.

DESIGN:

Final Bridge Design:

- Four alternative designs were considered for the final bridge design: an under truss, Howe truss, Pratt truss, and Warren truss.
- The alternative designs were modeled in the software *VisualAnalysis*
- The bridges were rated based on their total cost, which was dependent on the aggregate deflection, weight, and construction time. Table 1 shows the average total cost, based on the six load cases, for each alternative design.
- The Pratt truss was selected as the final design due to it having the lowest total cost in the table. A 3D isometric view of the preliminary final design can be seen in Figure 3.

Connection Design 1: (Figures 6 and 7)

- Connection Design #1 is a "Twist and Lock" design used to connect stringers, footing and lateral bracing members together.
- The connection will consist of four parts with two male and two female connectors.
- The bottom connectors will be attached first by dropping the male connectors disk into the female connector.
- The top male T- Slot connector will swing horizontally into the other stringers female connector.
- The bottom male connector has a small strip extruded out that the members will be capable of rotating, but large enough that the void space between the two members will be eliminated when it is rotated 90 degrees.
- This connection will be used 34 times in the design.
- Additional to members for the bolt requirement that will be offset 1.5" from the center of the stringers allowing a four inch steel bolt to be assembled through two of these apparatuses.

Connection Design 2: (Figure 8)

- Connection Design #2 is a sleeve design used to connect the overhead truss members.
- This design was selected to minimize the weight of the bridge by using a hollow connection.
- The overhead truss is under less stress than the stringers allowing us to use a weaker connection.
- Each member of the overhead truss will have a side which is slightly smaller than the pipe allowing it to slide into another member.
- This sleeve will have a total length of five inches with three inches welded inside the pipe and two inches extruding. This connection will be used 16 times in the design.
- The team decided to construct another external member to meet the bolt requirements that will consist of 4" of $\frac{1}{4}$ " diameter steel and 2" of $\frac{3}{8}$ " diameter steel.
- Allowing a four inch steel bolt to be assembled through two of these apparatuses eliminating any void space.

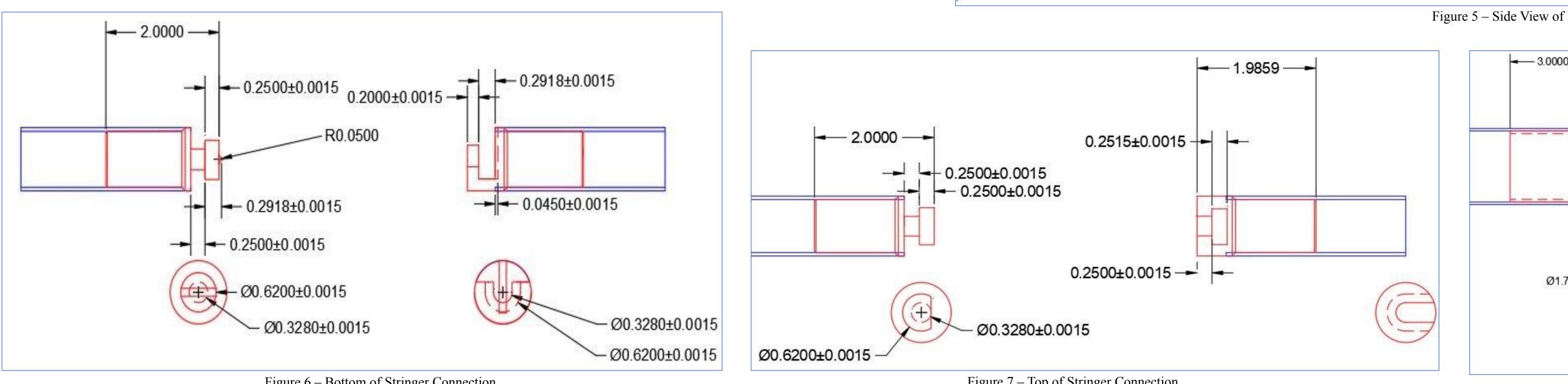
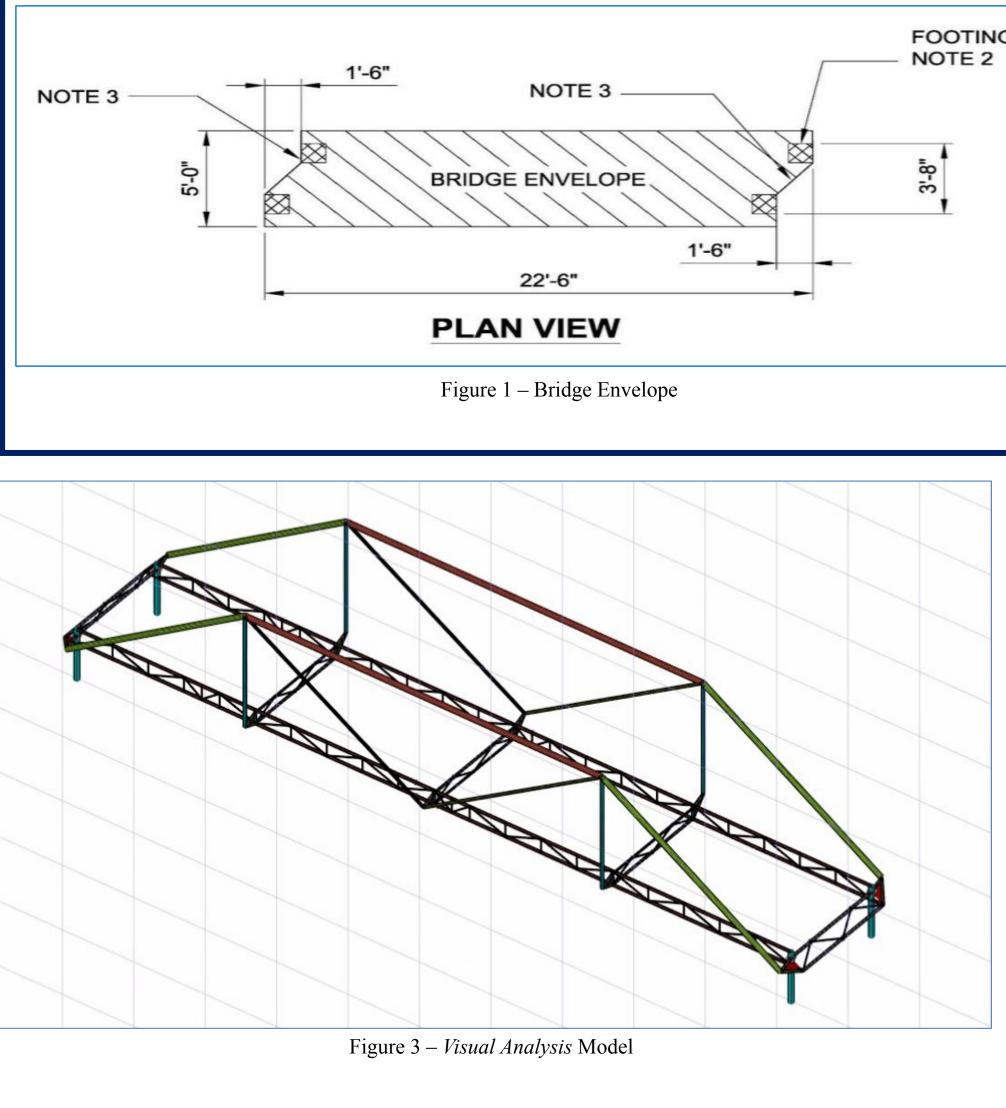
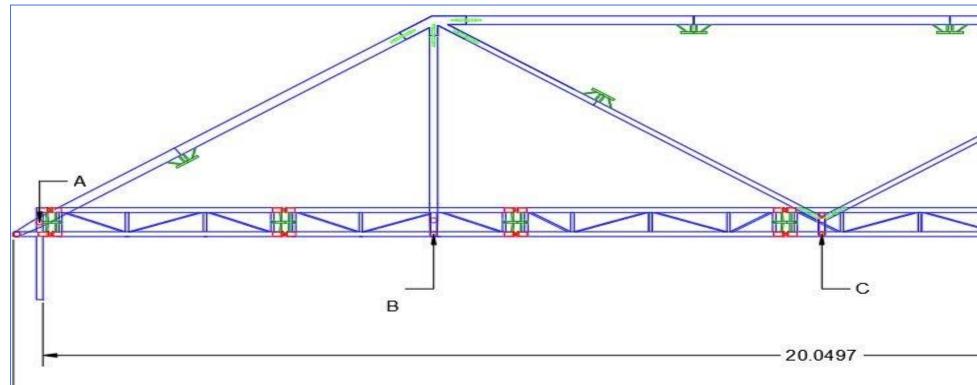


Figure 6 – Bottom of Stringer Connection

TCNJ 2021 AISC Steel Bridge Competition Andrew Agresto¹, Matthew Chaber¹, Steven Hippauf¹, Hunter Kelly¹, and Sofia Zapata¹ Advisors: Dr. Nabil Al-Omaishi¹ and Dr. James Maccariella¹ ¹Department of Civil Engineering, The College of New Jersey, Ewing NJ **RESULTS: DESIGN CONSTRAINTS:** Loading: • The bridge was subjected to a vertical load test and a lateral load test. • The bridge was subjected to a uniformly distributed load of 1500 lbs. and 1000 lbs. over three feet and a 50 lbs. lateral force. Aggregate De Size/Dimensions: Howe Truss • The total height was 4.87 feet above the ground and each stringer was between 3'-0" and 3'-6" feet long. Pratt Truss • The four footing boxes were 1' x 1' and offset by 1.5 feet on each side (Figure 1). Warren Truss Site Layout: Undertruss • The competition site was split into a right yard and a left yard, both yards contain tools, nuts, bolts, and builders and only the right yard was permitted to store bridge members. Maximum Shear (Kips.) Maxim 0.78 FOOTING (TYP.) NOTE 2 NOTE 3 SOUTH SIDE MEASURE D VERTICAL LOAD TEST PLAN PRELOAD -BRIDGE ENVELOPE - NORTH SIDE BEYOND 1'-6" SAFETY SUPPORT, TYP. 22'-6" **CONSTRUCTION SEQUENCING:** PLAN VIEW VERTICAL LOAD TEST ELEVATION **Construction Sequencing:** Figure 2 - Vertical Load Test Figure 1 – Bridge Envelope The bridge would be assembled in the order of footings, stringers, middle bracings of the lower truss, overhead truss assembly, and finally the bracings for the overhead assembly. The building process from bottom to top would provide for the greatest stability of the structure as upper members are attached. As each member is installed, the ideal sequence would require the - 3.9623 builder to immediately secure the connection with a bolt. The purpose of this would be to eliminate any slack that could be 3.7539 found in the joint and allow for easier handling as the assembly grows larger. Tools, Nuts and Bolts, are in both staging yards, while the bridge members are located only in the right staging yard. ٢ 4.8717 — 2.4532 — \bigcirc Tool 0.2851 Starting Configuration 0.0833 - 2.6312 - 0.0833 Figure 3 – Visual Analysis Model Figure 4 – Front View of Bridge Figure 9: Starting Configuration for Construction 4 871 D -20.0497 The footings and their associated lateral bracing are assembled 21.5091 Figure 5 – Side View of Bridge on both sides of the river Figure 10: Footings and Lateral Bracings are Placed -Ø1.7500±0.0015 Ø1.7500±0.001 Tools -Ø1.5090±0.0015 South side stringer is assembled and lateral bracing is installed - Ø1.6340±0.0015 Ø1.6340±0.0015 Figure 7 – Top of Stringer Connection Figure 8 – Overhead Truss Member Sleeve Connection





Acknowledgment: The team would like to thank the TCNJ School of Engineering and Civil Engineering Department, especially Dr. Al-Omaishi and Dr. James Maccariella Jr.. The team would also like to acknowledge the insight and resources provided by Joe Zanetti.

References:

(1) AISC Steel Bridge Competition Rules

(2) "VisualAnalysis V18 Edu." (2019). Home - VisualAnalysis, IES, Inc.,

Table 1: Alternative Design Evaluation									
eflection (In.)	Weight (lbs.)	Structural Cost (\$) Construc	tion time (minutes)	Construction Cost (\$)	Total Cost (\$)			
0.34	254	\$1,703,000	6	8.3	\$2,324,000	\$4,027,000			
0.29	256	\$1,561,500		8.3	\$2,324,000	\$3,885,500			
0.31	259	\$1,648,500		8.63	\$2,417,333	\$4,065,833			
0.77	231	\$2,873,500	5.82		\$1,628,667	\$4,502,167			
Table 2: Hand Calculated Results									
mum Moment (kipft)		gregate Deflection Range		Weight of Connect	tions (lbs.) Weight o	Weight of Bolts (lbs.)			
4.67		0.148 to 5.51		60	1	13.25			
Table 3: Hand Calculated Buckling Results General Buckling Flexural Buckling									

General	Ducking	FIEAUTAI DUCKIIIIg		
Capacity (kips.)	Max Force (kips.)	Capacity (kips.)	Max Force (kips.)	
2.2	1.36	1.94	1.36	



